

# Deconvolution-convolution treatment on powder diffraction data collected with Cu K $\alpha$ X-ray and Ni K $\beta$ filter

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A method to remove small Cu-K $\beta$  peaks and step structures caused by Ni K-edge absorption as well as Cu-K $\alpha_2$  sub-peaks from powder diffraction intensity data measured with Cu-target X-ray source and Ni-foil filter is proposed. The method is based on deconvolution-convolution treatment applying scale transform of abscissa, Fourier transform, and a realistic spectroscopic model for the source X-ray. The validity of the method has been tested by analysis of the powder diffraction data of a standard LaB<sub>6</sub> powder (NIST SRM660a) sample, collected with the combination of Cu-K $\alpha$  X-ray source, Ni-foil K $\beta$  filter, flat powder specimen and one-dimensional Si strip detector. The diffraction intensity data treated with the method have certainly shown background intensity profile without Cu-K $\beta$  peaks and Ni K-edge step structures.

Keywords: Cu K-emission, Ni K $\beta$  filter, bremsstrahlung, deconvolution, convolution

## I. INTRODUCTION

One of the reasonable configurations for laboratory powder diffraction measurement systems is currently the combination of (i) a Cu-target sealed tube in the orientation of line-focus geometry, (ii) a couple of Soller slits on the incident and diffracted beam sides, (iii) Ni-foil K $\beta$  filter, (iv) flat powder specimen and (v) Si strip one-dimensional

(1D) detector. Since the transmittance of the Ni foil of 0.02 mm in thickness is about 0.44 for Cu-K $\alpha$  and 0.007 for Cu-K $\beta$  X-rays, insertion of a Ni foil effectively reduces the diffraction peak caused by Cu-K $\beta$  emission from the Cu-target X-ray tube. The use of a Johan-type or Johanson-type monochromator, or a graded multilayer mirror on the incident beam side, or a curved graphite analyzer on the diffracted beam side, may be another possible choice to remove Cu-K $\beta$  peaks. However, the use of a monochromator, multilayer mirror or analyzer generally causes theoretical complexity for modeling the spectroscopic characteristics of the source X-ray, because mutual correlation between the direction and wavelength of the X-ray beam should be introduced by such a diffractive optical element (Toraya and Hibino, 2000). Furthermore, only slight misalignment of a diffractive optical element may cause severe distortion of the observed diffraction peak profile (Ida *et al.*, 2001).

We have previously demonstrated that Cu-K $\alpha_2$  sub-peaks can be removed by a deconvolution-convolution method, from the diffraction intensity data collected with a conventional laboratory powder diffractometer, where the diffracted beam intensities measured on the diffraction angle,  $2\theta$ -scale of abscissa, are mapped onto the scale-transformed abscissa,  $x \equiv \ln \sin \theta$ . This article is intended to demonstrate that the method is also effective to remove both Cu-K $\beta$  sub-peaks and Ni K-edge step structures from the powder diffraction data collected with a laboratory powder diffraction measurement system with a Ni-foil filter.

## II. THEORETICAL

A deconvolution-convolution method to remove the effects of axial-divergence, flat-specimen and sample-transparency aberrations in Bragg-Brentano geometry has been described in our previous report (Ida and Toraya, 2002). The details of slight improvement about the treatment of axial-divergence aberration, which has already been applied in this study, will be discussed elsewhere (Ida *et al.*, submitted). This article is focused on the methodology to remove Cu-K $\alpha_2$  and K $\beta$  peaks and Ni K-edge structures from experimental data.

## A. Scale transform of abscissa

When the diffraction intensity profile is plotted on the abscissa scale of  $x = \ln \sin \theta$  instead of the diffraction angle  $2\theta$ , whole powder diffraction data can be expressed as the convolution with the common spectroscopic profile function of source X-ray (Ida and Toraya, 2002). Figure 1 illustrates the core idea about the scale transform.

Observed powder diffraction profile of  $\text{LaB}_6$  is plotted on the diffraction angle  $2\theta$  in Figure 1(a), and Figure 1(b) plots exactly the same intensity data on the natural logarithm of  $\sin \theta$ . Each of reflection peaks is composed of  $K\alpha_1$  and  $K\alpha_2$  peaks, and the separation of the  $K\alpha_1$  and  $K\alpha_2$  peaks varies on the horizontal scale of  $2\theta$ , while it is constant on the horizontal scale of  $x = \ln \sin \theta$ . In other words, the diffraction intensity profile is expressed by the convolution with the common instrumental function about spectroscopic profile of the source X-ray on the scale of  $x = \ln \sin \theta$ , but it is not a convolution on the scale of  $2\theta$ .

When the observed data are given by a set of diffraction angles and intensities  $(2\theta, I)$ , the abscissa and ordinate values are changed to  $(x, y)$  by the following equations,

$$x = \ln \sin \theta, \quad (1)$$

$$y = 2IC(2\theta) \tan \theta, \quad (2)$$

where  $C(2\theta)$  is the geometric correction factor given by

$$C(2\theta) = \frac{2 \sin \theta \sin 2\theta}{1 + \cos^2 2\theta}, \quad (3)$$

for a Bragg-Brentano powder diffractometer without a diffractive optical element.

After the scale-transformed data  $(x, y)$  are changed to  $(x', y')$  by the deconvolution-convolution process, the intensity will be treated by

$$I' = \frac{y'}{2C(2\theta) \tan \theta}, \quad (4)$$

to obtain the modified intensity data on the original  $2\theta$ -scale,  $(2\theta, I')$ .

## B. Emission of Cu-target X-ray

Assuming the peak energy and wavelength of the Cu-K $\alpha_1$  emission to be  $E_{\alpha 1} = 8.04783$  keV (Deutsch *et al.*, 2004) and  $\lambda_{\alpha 1} = 1.5405929$  Å, we here apply the transformation given by

$$x = \ln \frac{E_{\alpha 1}}{E} = \ln \frac{\lambda}{\lambda_{\alpha 1}}, \quad (5)$$

for arbitrary photon energy  $E$  and wavelength  $\lambda$ . A model for spectroscopic profile of the source X-ray,  $f_X(x)$ , is given by

$$f_X(x) = f_\alpha(x) + S_{\beta/\alpha} f_\beta(x) + S_B(x), \quad (6)$$

where  $f_\alpha(x)$  and  $f_\beta(x)$  are the normalized Cu-K $\alpha$  and K $\beta$  emission peak profile functions,  $S_{\beta/\alpha}$  the Cu-K $\beta$ /Cu-K $\alpha$  intensity ratio, and  $S_B(x)$  the contribution of the white X-ray caused by bremsstrahlung.

The Cu-K $\alpha$  emission peak profile is expressed by

$$f_\alpha(x) = \sum_{i=1}^2 \sum_{j=1}^2 \frac{2I_{\alpha ij}}{\pi \Delta x_{\alpha ij}} \left[ 1 + 4 \left( \frac{x - x_{\alpha ij}}{\Delta x_{\alpha ij}} \right)^2 \right]^{-1}, \quad (7)$$

$$x_{\alpha ij} = \ln \frac{E_{\alpha 1}}{E_{\alpha ij}} \approx \frac{E_{\alpha 1} - E_{\alpha ij}}{E_{\alpha 1}}, \quad (8)$$

$$\Delta x_{\alpha ij} \approx \frac{W_{\alpha ij}}{E_{\alpha ij}}, \quad (9)$$

where the values of intensity  $I_{\alpha ij}$ , location  $E_{\alpha ij}$  and peak width  $W_{\alpha ij}$  of the component Lorentzian functions given in a literature (Deutsch *et al.*, 2004) are listed in Table I.

The Cu-K $\beta$  emission peak profile is similarly expressed by

$$f_\beta(x) = \sum_{i=1}^5 \frac{2I_{\beta i}}{\pi \Delta x_{\beta i}} \left[ 1 + 4 \left( \frac{x - x_{\beta i}}{\Delta x_{\beta i}} \right)^2 \right]^{-1}, \quad (10)$$

$$x_{\beta i} = \ln \frac{E_{\alpha 1}}{E_{\beta i}}, \quad (11)$$

$$\Delta x_{\beta i} \approx \frac{W_{\beta i}}{E_{\beta i}}, \quad (12)$$

where the values of component intensity  $I_{\beta i}$ , location  $E_{\beta i}$  and peak width  $W_{\beta i}$  are also listed in Table I.

The contribution of white X-ray,  $S_B(x)$  in Eq. (6), should be dependent on (i) the acceleration voltage and target material of the X-ray tube, (ii) absorption and scattering of beryllium window of the sealed tube and atmosphere through the X-ray beam path from the X-ray source to the detector, (iii) energy-dependent sensitivity of the detector, and also (iv) the settings of the pulse-height discriminator or analyzer.

Trincavelli *et al.* (1998) have proposed a formula for the spectroscopic distribution of the bremsstrahlung given by

$$\frac{\Delta I}{\Delta E} = \sqrt{Z} \frac{E_0 - E}{E} \left[ -54.86 - 1.072E + 0.2835E_0 + 30.4 \ln Z + \frac{875}{Z^2 E_0^{0.08}} \right], \quad (13)$$

where  $Z$  is the atomic number of the target material,  $E_0$  the upper limit of the photon energy in the unit of keV, and  $E$  the photon energy of the X-ray. The intensity distribution on the scale of  $x = \ln(E_{\alpha 1}/E)$  is calculated from  $\Delta I/\Delta E$  by

$$\frac{\Delta I}{\Delta x} = \frac{E \Delta I}{\Delta E}. \quad (14)$$

Figure 2 shows the intensity distribution of the bremsstrahlung calculated by Eq. (13) for Cu target and  $E_0 = 45$  keV, multiplied by the transmittance of air (4:1 mixture of nitrogen and oxygen) through the path of 480 mm in length, which is calculated by the Cromer-Liberman algorithm (Cromer, 1981; Cromer and Liberman, 1983).

Here we apply a simplified model for the white X-ray intensities, the normalized formula of which is given by

$$S_B(x) = \begin{cases} \frac{I_B}{N} \left( \frac{x - x_0}{\Delta x_B} \right) \operatorname{erfc} \left( \frac{x - x_B}{\Delta x_B} \right) & [x_0 < x] \\ 0 & [x \leq x_0] \end{cases}, \quad (15)$$

$$N = \frac{\Delta x_B}{4} \left[ (1 + 2t_0^2) \operatorname{erfc}(t_0) - \frac{2t_0}{\sqrt{\pi}} \exp(-t_0^2) \right], \quad (16)$$

$$t_0 = \frac{x_0 - x_B}{\Delta x_B}, \quad (17)$$

where the integrated intensity of white X-ray  $I_B$ , and the profile parameters  $x_B$  and  $\Delta x_B$  are treated as adjustable parameters. The lower limit on the scale of  $x$ ,  $x_0 = \ln(E_{\alpha_1}/E_0)$ , which corresponds to the upper limit of the photon energy, may appear to be treated as a fixed parameter determined by the acceleration voltage, but the value can be changed in practical application, because it is likely that the upper limit of the photon energy of the white X-ray to be detected is restricted by the energy-dependent sensitivity of the detector rather than the acceleration voltage. The intensity profile calculated by Eqs. (15)–(17) is also shown in Figure 2. Note that almost linear dependence of the peak profile of the function  $S_B(x)$  on the side of smaller  $x$  is dominantly determined by the bremsstrahlung characterized by the parameter  $x_0$ , but the intensity for larger  $x$  is assumed to be restricted by the extinction by the air, and simulated by adjusting the values of the parameters  $x_B$  and  $\Delta x_B$ .

### C. Effect of Ni filter for Cu K-emission X-ray source

When a Ni foil is used as a  $K\beta$  filter, the virtual spectroscopic profile of the source X-ray,  $f_{X:Ni}(x)$ , should be given by

$$f_{X:Ni}(x) = T_{Ni}(x)f_X(x), \quad (18)$$

where  $T_{Ni}(x)$  is the transmittance spectrum of the Ni foil, given by

$$T_{Ni}(x) = \exp[-(\mu/\rho)_{Ni}(x)\rho_{Ni}t_{Ni}], \quad (19)$$

where  $\rho_{Ni}$  and  $t_{Ni}$  are the density and thickness of the Ni foil, respectively, and  $(\mu/\rho)_{Ni}(x)$  is the mass absorption coefficient spectrum of Ni. The spectrum of  $(\mu/\rho)_{Ni}(x)$  calculated by the method of Cromer and Liberman (Cromer, 1983; Cromer and Liberman, 1981) is further simplified here by the following equation,

$$(\mu/\rho)_{Ni}(x) = \begin{cases} 337.58 \exp[2.7130(x - x_{Ni-K})] & [x < x_{Ni-K}] \\ 41.145 \exp[2.8097(x - x_{Ni-K})] & [x_{Ni-K} \leq x] \end{cases}, \quad (20)$$

where  $x_{Ni-K} = -0.03478$  is the location of Ni K-absorption edge ( $E_{Ni-K} = 8.3327$  keV) relative to the Cu  $K\alpha_1$  peak position.

Figure 3 compares the mass absorption coefficient spectrum calculated by the Cromer-Liberman method and the simplified formula given by Eq. (20). No significant

difference between the Cromer-Lieberman profile and the profile calculated by Eq. (20) can be detected in the range displayed in Figure 3.

#### D. Hypothetical Cu $K\alpha_1$ singlet spectrum without Ni K-absorption edge

Removal of Cu- $K\alpha_2$ ,  $K\beta$  sub-peaks and Ni K-edge structure can be achieved by deconvolution of the realistic spectroscopic profile modeled in the sections II.B and II.C, and convolution with a hypothetical spectroscopic profile of a Cu- $K\alpha_1$  singlet, the model for which will be described in this section.

Hypothetical Cu- $K\alpha_1$  singlet spectrum without Ni K-absorption edge is expressed by

$$f_{X::Ni^*}(x) = T_{Ni^*}(x)f_{X^*}(x) , \quad (21)$$

where  $T_{Ni^*}(x)$  is the transmittance spectrum given by

$$T_{Ni^*}(x) = \exp[-(\mu/\rho)_{Ni^*}(x)\rho_{Ni}t_{Ni}] , \quad (22)$$

where  $(\mu/\rho)_{Ni^*}(x)$  is the hypothetical mass absorption coefficient spectrum of Ni without K-absorption edge, given by

$$(\mu/\rho)_{Ni^*}(x) = 41.145 \exp[2.8097(x - x_{Ni-K})] . \quad (23)$$

As can be seen in the spectrum calculated by Eq. (23) plotted in Figure 3, it is just extrapolation of the spectroscopic profile of Ni in the lower energy (larger  $x$ ) region.

The function  $f_{X^*}(x)$  in Eq. (21) is a Cu- $K\alpha_1$  singlet spectrum, which we here assume to be

$$f_{X^*}(x) = f_{\alpha_1}(x) + f_B S_B(x) , \quad (24)$$

where  $f_{\alpha_1}(x)$  is given by

$$f_{\alpha_1}(x) = \frac{2I_{\alpha_1}}{\pi\Delta x_{\alpha_1}} \left[ 1 + 4 \left( \frac{x - x_{\alpha_1}}{\Delta x_{\alpha_1}} \right)^2 \right]^{-1} , \quad (25)$$

which is identical to the  $K\alpha_1$  component in the  $K\alpha_1$ ,  $K\alpha_2$  doublet model (see Table I).

The parameter  $f_B$  in Eq. (24) is a factor to adjust the background in the output data. When the white background is fully removed from the input data and not added to the output ( $f_B = 0$ ), it is likely that negative intensities will be created in the background region because of the statistical variation of the observed intensities. Although there will be no reason not to allow negative intensities when the statistical errors are

explicitly assumed in subsequent analysis of data, it may be difficult for some users of traditional codes for Rietveld analysis (Rietveld, 1969) to include explicit error values in their analyses. On the other hand, when the white background is fully added ( $f_B = 1$ ), the background intensities in the output data should naturally be enhanced, because we here assume higher transmittance of Ni without K-absorption as defined by Eq. (23).

## E. Deconvolution and convolution treatments

In our previous report (Ida and Toraya, 2002), we have applied the analytical formula for the Fourier transform of the spectroscopic distribution of the source X-ray. In this study, the Fourier transforms of the model functions are numerically calculated applying the following formulas,

$$F_{X:Ni}(k) = \sum_{j=-n/2}^{n/2-1} f_{X:Ni}(j\Delta x) \exp\left(\frac{2\pi i k j}{n}\right), \quad (26)$$

$$F_{X*:Ni*}(k) = \sum_{j=-n/2}^{n/2-1} f_{X*:Ni*}(j\Delta x) \exp\left(\frac{2\pi i k j}{n}\right), \quad (27)$$

where  $\Delta x$  is the step interval of the sampling points. The values of  $\Delta x$  and  $n$  should be determined not to lose information included in the source data and to keep sufficient width of marginal region to reduce the end effects (Ida and Toraya, 2002).

The deconvolution-convolution process about intensities  $y_j \rightarrow y'_j$  is expressed by

$$y'_j = \frac{1}{n} \sum_{k=-n/2}^{n/2} \frac{F_{X*:Ni*}(k)}{F_{X:Ni}(k)} Y_k \exp\left(-\frac{2\pi i k j}{n}\right), \quad (28)$$

$$Y_k = \sum_{j=0}^{n-1} y_j \exp\left(\frac{2\pi i k j}{n}\right), \quad (29)$$

where the values of  $y_j$  in Eq. (29) are intensity values for the sampling points of  $x_j = x_0 + j\Delta x$ , evaluated by cubic-spline interpolation of the source data. Marginal data in the range  $x_0 + m\Delta x < x_j < x_0 + n\Delta x$  for  $x_0 + m\Delta x \approx \ln \sin \theta_{\max}$  were filled with the values given by the following equation,



$$y_j = \begin{cases} y_m & \left[ m < j < \frac{2m+n}{3} \right] \\ \frac{(2n+m-3j)y_m + (3j-2m-n)y_0}{n-m} & \left[ \frac{2m+n}{3} < j < \frac{m+2n}{3} \right] \\ y_0 & \left[ \frac{m+2n}{3} < j < n \right] \end{cases}. \quad (30)$$

The fast Fourier transform algorithm can be used for all the calculations of Eqs. (26)–(29).

### III. EXPERIMENTAL

#### A. Sample

Standard LaB<sub>6</sub> powder (NIST SRM660a) was used as received. The powder was filled into the cavity of a flat glass holder with the capacity of 0.1152 mL and the rectangular cross section of 20 × 15 mm<sup>2</sup> (average depth of 0.384 mm). The filling factor of the powder was estimated at 26.7 % by weight measurement, and the penetration depth of the CuK $\alpha$  X-ray into the powder sample was estimated at  $\mu^{-1} = 0.044$  mm.

#### B. Data collection

Diffraction data were collected with a powder diffractometer (PANALytical, X'Pert PRO MPD) with a Cu-target sealed tube,  $\theta$ - $\theta$  type goniometer (PANALytical, PW3050/60) equipped with a one-dimensional Si strip detector (PANALytical X'Celerator). The X-ray source and the detector are symmetrically located at the distance of 240 mm from the rotation axis of the goniometer. The X-ray tube was operated at the voltage of 45 kV and the current of 40 mA. Fixed-angle divergence slit of 0.5° and a couple of Soller slits with the open angle of 0.04 rad were used. Ni foil of 0.02 mm in thickness was used as a K $\beta$  filter. The one-dimensional powder diffraction intensity data of 8,079 sampling points were created by an automatic measurement / data processing program (PANALytical, Data Collector) from the integration of 5 iterations of continuous scan for the diffraction angles ranging from 10° to 145° with the nominal step interval of 0.0167° and nominal measurement time of 10.16 s per step. The total measurement time for data collection was about 1h.

#### IV. RESULTS AND DISCUSSION

Figure 4 shows the background intensity profile of LaB<sub>6</sub> (NIST SRM660a) and the deconvolved-convolved intensity profile calculated on some variation of parameters, (i) the upper limit of X-ray photon energy,  $E_0$  and (ii) the output white X-ray level,  $f_B$ , while other adjustable parameters for the model of white X-ray are fixed as follows, (iii) Cu K $\beta/\alpha$  intensity ratio  $S_{\beta/\alpha} = 0.2$ , (iv) white X-ray intensity relative to Cu-K $\alpha_1$ ,  $I_B = 0.4$ , (v) relative location of the decay of the white X-ray on the lower energy side,  $x_B = 0.17$ , and (vi) the decay-width parameter,  $\Delta x_B = 0.48$ .

It should be noted that the Cu-K $\alpha_2$  peaks have effectively been removed in the deconvolved-convolved data, just by applying the parameters proposed by Deutsch *et al.* (2014) without any modification or adjustment. As can be seen in Figure 4(b) and (c), severe deformation of the background profile has appeared in the deconvolved-convolved data, when the upper limit of the photon energy  $E_0$  is set to the acceleration voltage of 45 keV. Hereafter,  $E_0 = 10$  keV and  $f_B = 0$  are assumed, because both Cu-K $\beta$  peaks and Ni K-edge structures are effectively removed without deformation of the background profile in the deconvolved-convolved data calculated for those values, as shown in Figure 4(d).

Figure 5 compares the background intensity profile of the (a) observed and (b) deconvolved-convolved data in the lower-angle region including 100, 110 and 111-reflection peaks of LaB<sub>6</sub>. The calculated locations of K $\beta$  peaks and Ni K-absorption edges for 100, 110 and 111-reflections are marked by vertical arrows in Figure 5. Since the reduction of K $\beta$  peaks is simply achieved by adjusting the value of Cu K $\beta/\alpha$  intensity ratio  $S_{\beta/\alpha}$  without changing other parameters, there is almost no ambiguity about the assumed value of  $S_{\beta/\alpha} = 0.2$ .

There still remains ambiguity to determine the parameters to characterize the observed white X-ray profile,  $x_0$ ,  $I_B$ ,  $x_B$  and  $\Delta x_B$ , which should be dependent on the extinction of the X-ray and/or sensitivity of the detector, rather than the intrinsic spectroscopic profile of bremsstrahlung. We have assumed  $x_B = 0.17$  and  $\Delta x_B = 0.48$  based on the simulation of the extinction by air through the total beam path of 480 mm in length,

as described in section II B, and neglected the absorption of beryllium window and sensitivity of the detector. The value of integrated intensity of the white X-ray, assumed to be  $I_B = 0.4$ , effectively reduces the step structure caused by Ni K-absorption edge, as can be seen in Figure 5(b), but it should also be dependent on the values of  $x_B$  and  $\Delta x_B$ .

Figure 6 shows the spectroscopic profile of  $f_{X:Ni}(x)$  and  $f_{X*:Ni*}(x)$  used for deconvolution and convolution, respectively. The profile  $f_{X:Ni}(x)$  includes the contribution of the white X-ray, but the profile  $f_{X*:Ni*}(x)$  does not include white X-ray ( $f_B = 0$ ). It should be noted that the step structure caused by Ni K-edge absorption is primarily due to the white X-ray and the contribution of the tails of  $K\alpha$  emission peak intensities at the points of Ni K-absorption edge is not large. Since there is no restriction for the hypothetical profile model  $f_{X*:Ni*}(x)$ , a more appropriate model may be derived, if a more realistic model for the spectroscopic profile of white X-ray is known.

The deconvolution-convolution treatment looks advantageous particularly for the data measured with a Ni-foil  $K\beta$ -filter. The treatment can also simplify subsequent analysis, such as individual peak profile fitting or whole pattern fitting, because of the smoothed background and the  $K\alpha_1$  singlet peak profile, the latter of which will be simulated by a simple profile function.

The use of a convolved (FPA) peak profile model may still be an alternative to the deconvolution-convolution method, but the application of the FPA method to individual peak profile fitting will become more restricted, if the Cu- $K\beta$  or Ni K-edge structures in the observed intensity profile cannot be neglected.

## V. CONCLUSION

Powder diffraction intensity data of standard  $LaB_6$  powder measured with Cu- $K\alpha$  X-ray source and Ni-foil  $K\beta$  filter have been treated by a deconvolution-convolution method based on the abscissa-scale transform and Fourier transform calculations. A Cu- $K\alpha$  quartet model with asymmetric  $K\alpha_1$  and  $K\alpha_2$  peak profile, and a Cu- $K\beta$  quintet model

have been incorporated in the model on the deconvolution, and a hypothetically symmetric  $K\alpha_1$  singlet profile has been applied on the convolution. There still remains ambiguity for treatment of the contribution of the white X-ray generated by bremsstrahlung, which is necessary to be considered for removal of Ni K-edge structures, but the removal of Cu- $K\alpha_2$  and Cu- $K\beta$  peaks is quite straightforward in the theoretical framework of this method.

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TABLE I. Peak energy  $E$ , full width at half maximum  $W$  and integrated intensity  $I$  for doublet and quartet models for Cu-K $\alpha$  emission and a quintet model for Cu-K $\beta$  emission (Deutsch *et al.*, 2004).

Model	Component	$E$ (eV)	$W$ (eV)	$I$
Cu-K $\alpha$ doublet	$\alpha_1$	8047.83(1)	2.29(2)	0.659
	$\alpha_2$	8027.85(1)	3.34(6)	0.341
Cu-K $\alpha$ quartet	$\alpha_{11}$	8047.837(2)	2.285(3)	0.579
	$\alpha_{12}$	8045.367(22)	3.358(27)	0.080
	$\alpha_{21}$	8027.993(5)	2.666(7)	0.236
	$\alpha_{22}$	8026.504(14)	3.571(23)	0.105
Cu-K $\beta$ quintet	$\beta_a$	8905.532(2)	3.52(1)	0.485
	$\beta_b$	8903.109(10)	3.52(1)	0.248
	$\beta_c$	8908.462(20)	3.55(3)	0.110
	$\beta_d$	8897.387(50)	8.08(8)	0.100
	$\beta_e$	8911.393(57)	5.31(8)	0.055

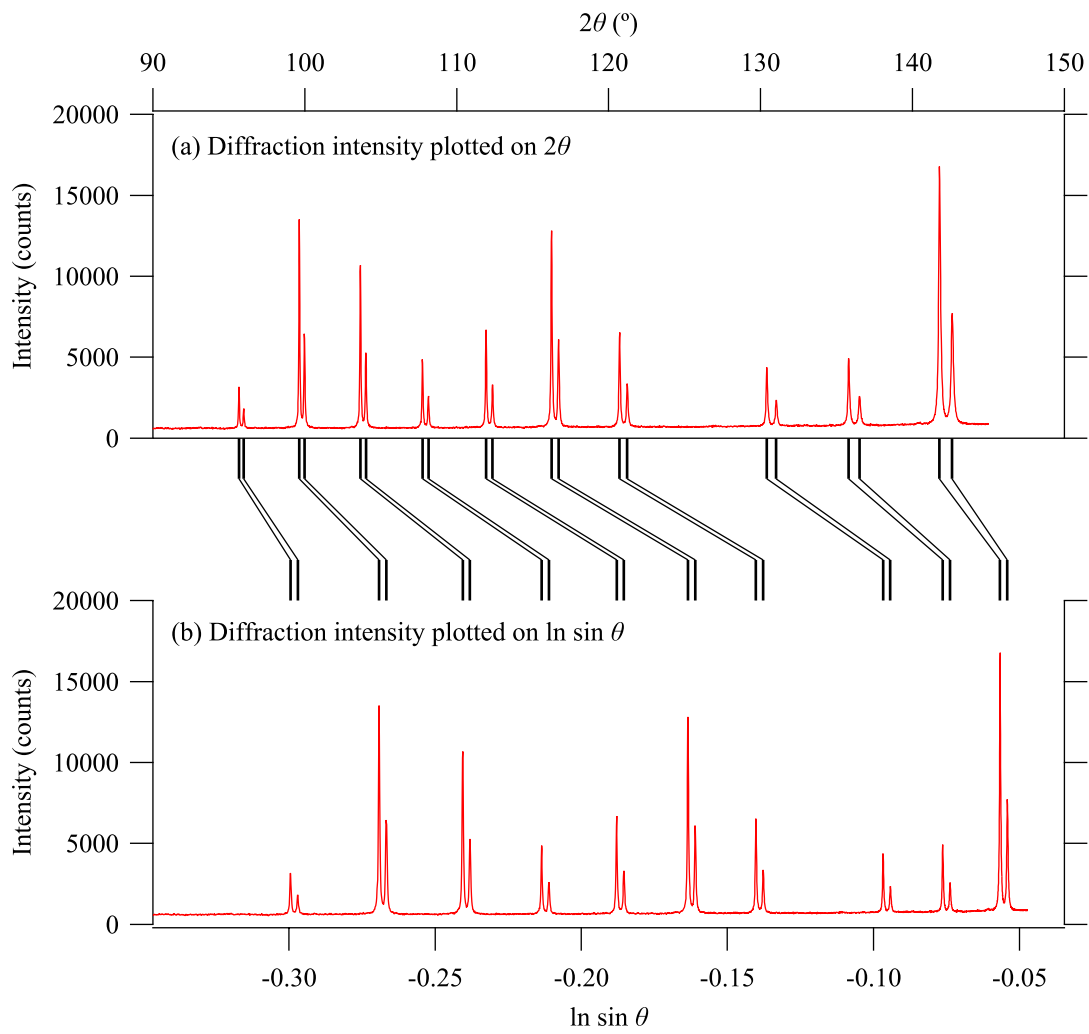


Figure 1 Diffraction intensity data of  $\text{LaB}_6$  plotted on (a)  $2\theta$  and (b)  $\ln \sin \theta$ .

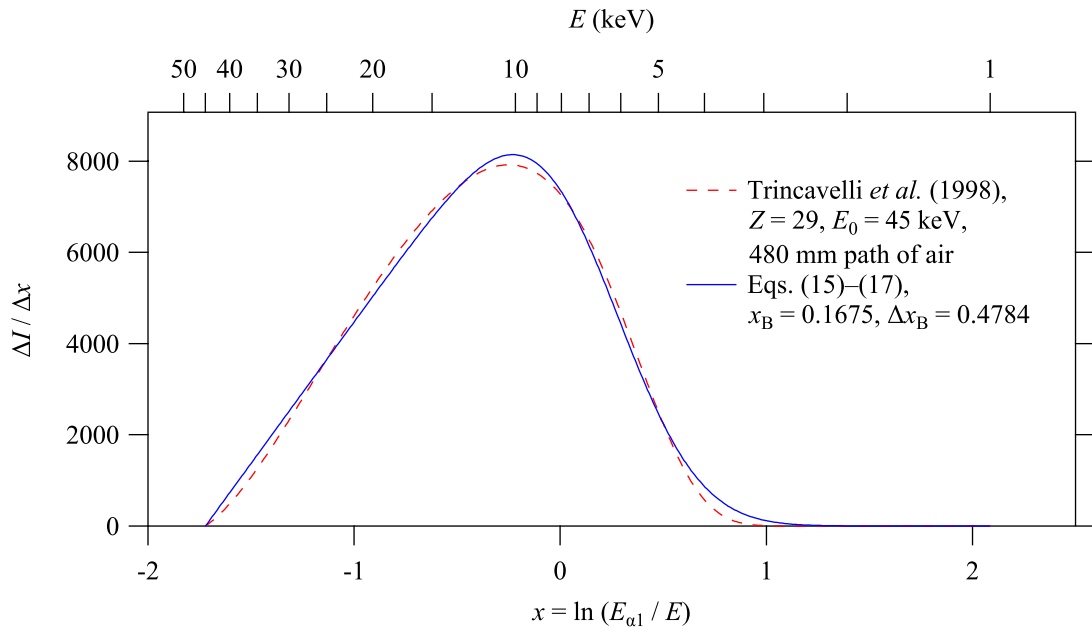


Figure 2 White X-ray (bremsstrahlung) spectra calculated by the formula of Trincavelli *et al.* (1998) and Eqs. (15)–(17).

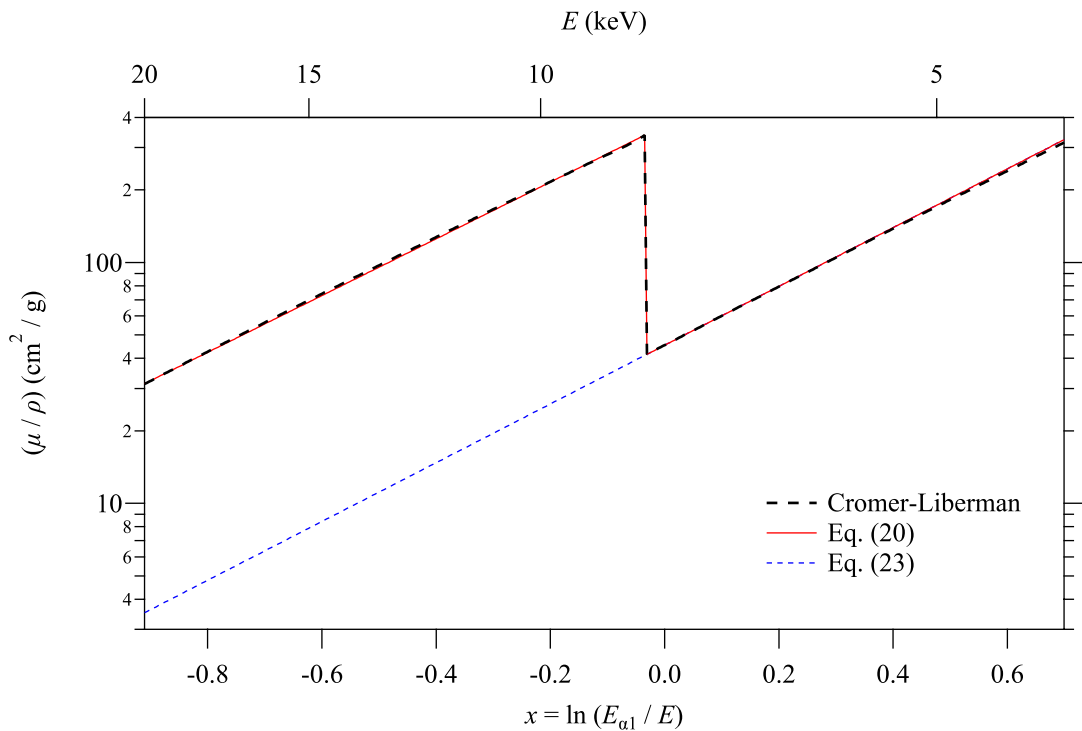


Figure 3 Comparison of the mass absorption coefficient spectra of Ni calculated by the Cromer-Liberman method (thick broken line), a simplified model (thin solid line), and the hypothetical spectrum without K-absorption edge.

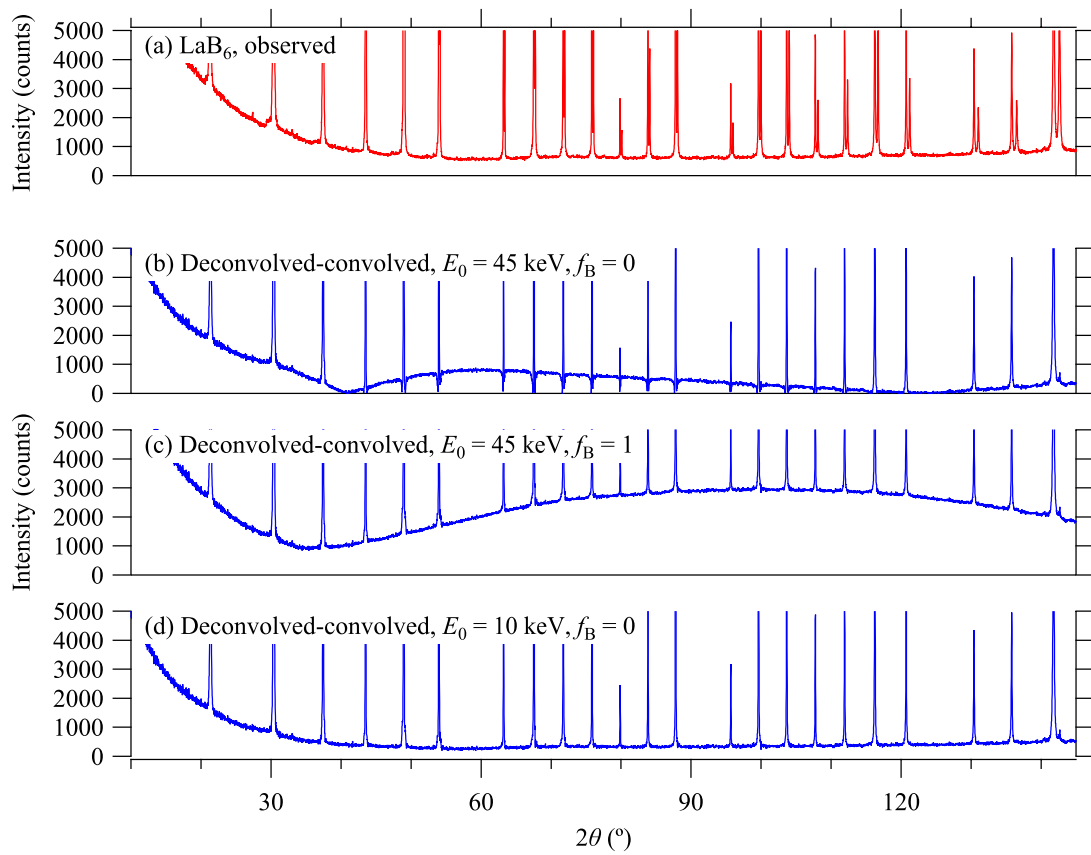


Figure 4 (a) Overall background profile of observed diffraction data of LaB<sub>6</sub> powder measured with a Cu-target X-ray tube and Ni-foil K $\beta$  filter, and the deconvolved-convolved data calculated with the parameters (b)  $E_0 = 45$  keV and  $f_B = 0$ , (c)  $E_0 = 45$  keV and  $f_B = 1$ , (d)  $E_0 = 10$  keV and  $f_B = 0$ .



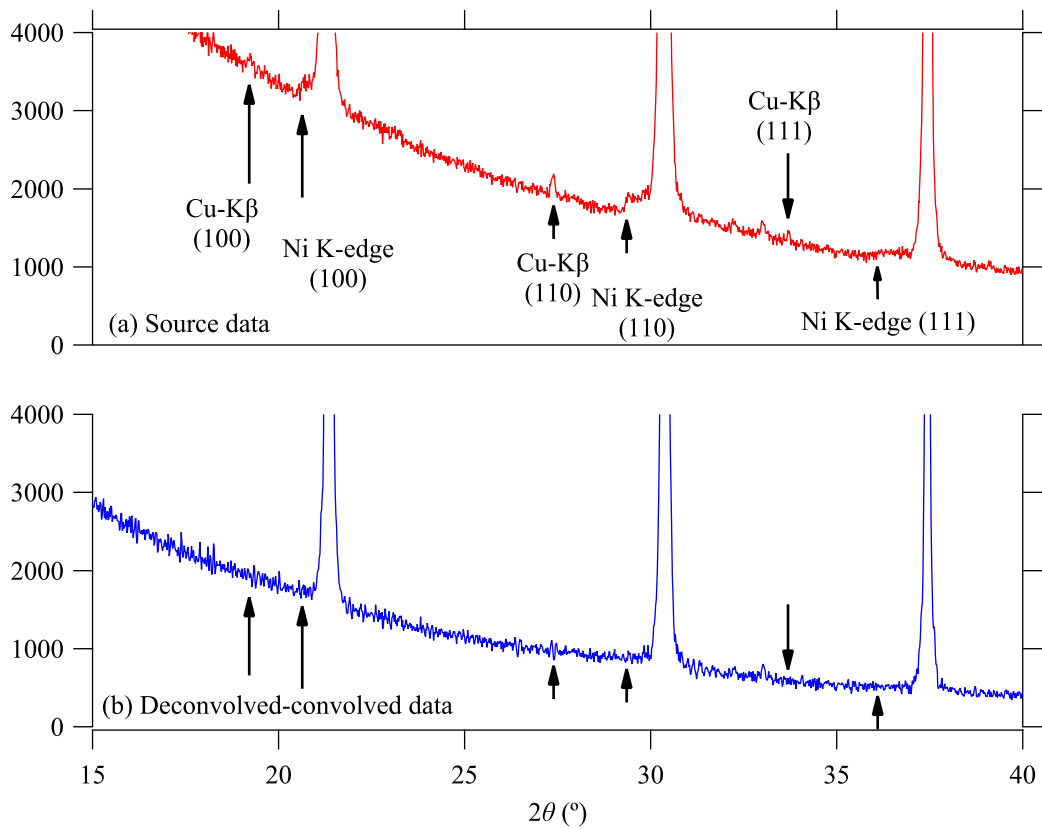


Figure 5 Background intensity profile of the (a) observed and (b) deconvolved-convolved data in lower diffraction angle.

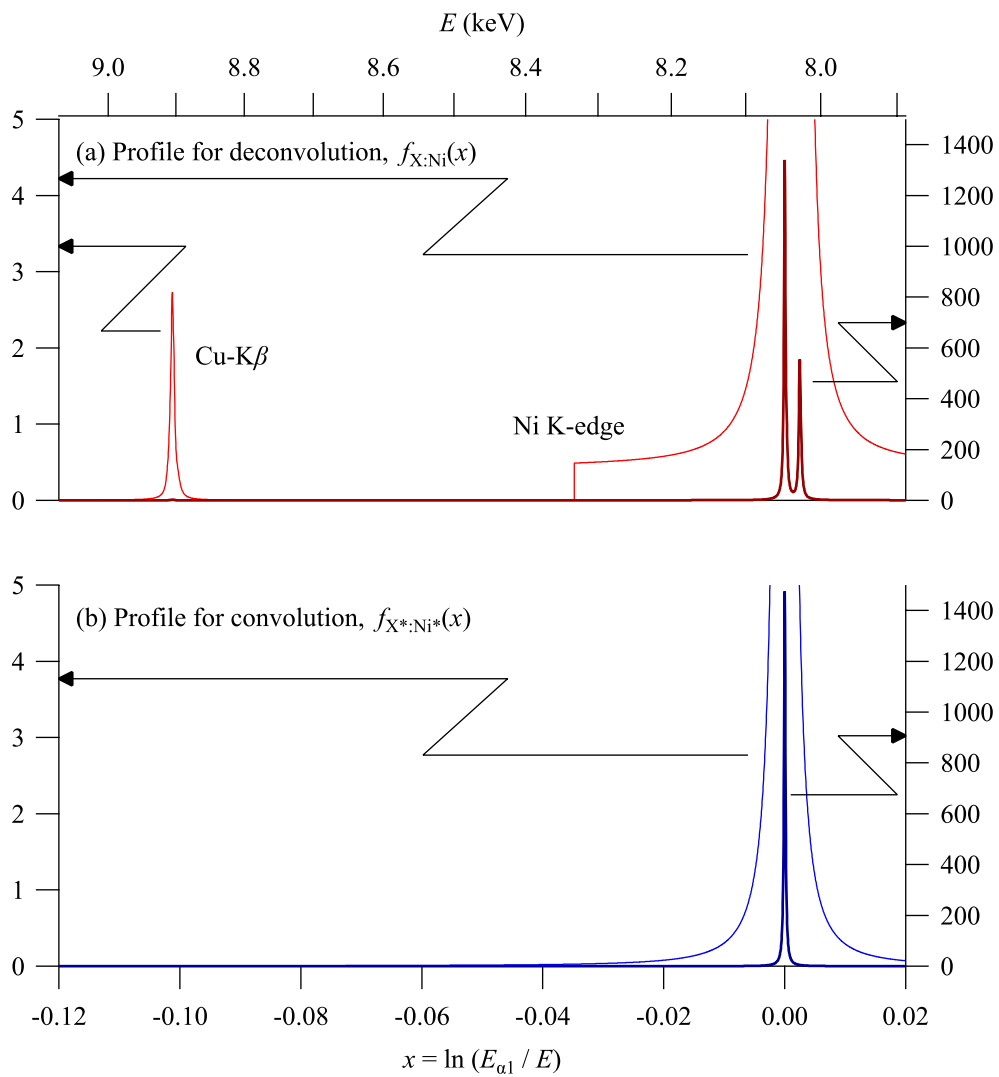


Figure 6 Spectroscopic profile used for (a) deconvolution and (b) convolution.